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Stelsiem en Regeltechniek FMT / Mechatronica

Deel 4: Stabiliteit van regelsystemen Blok 8: Stabiliteit van regelsystemen - Theorie

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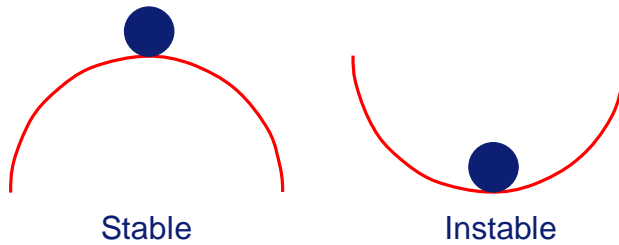
Cursus Stelsiem en Regeltechniek Overzicht

Deel 1	Blok 1. Inleiding
Wo. 14-04	Blok 2. Basisprincipes modelvorming massa-veersystemen
	Blok 3. De regelaar als veer-demper combinatie
Deel 2	Blok 4. Frequentie-domein beschrijving
Wo. 21-04	Blok 5. Basisconcepten in de regeltheorie
Deel 3	Blok 6. Verdere inleiding in de regeltheorie
Wo. 28-04	Blok 7. De PD regelaar als veer-demper combinatie
Deel 4	Blok 8. Stabiliteit van regelsystemen
Wo. 12-05	Blok 9. De PID regelaar in het frequentie domein
Deel 5	Toepassing: PID regelaarontwerp
Wo. 19-05	
Deel 6	Extra regeltechniek
Wo. 26-05	

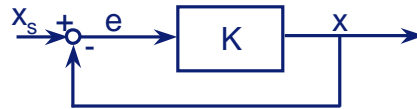
Why becomes a control system unstable?



Introduction



Introduction



$$\frac{x}{x_s} = \frac{K}{1+K}$$

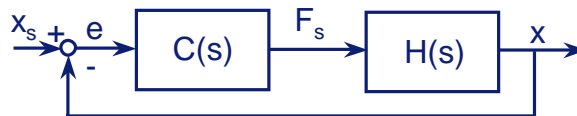
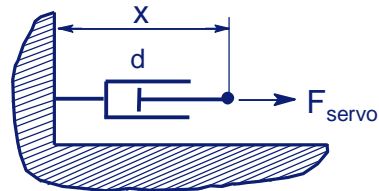
K	0	1	-1
x/x _s	0	0.5	∞

Introduction

Transfer functions:

$$H(s) = \frac{x(s)}{F(s)} = \frac{1}{ds}$$

$$C(s) = \frac{F(s)}{e(s)} = k_p$$



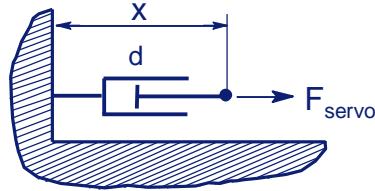
$$\frac{x}{x_s} = \frac{k_p/ds}{1+k_p/ds} = \frac{1}{d/k_p \cdot s + 1} = \frac{1}{\tau s + 1}$$

When stable?

Stability in the time domain

First order system
(damper with P controller):

$$y = \frac{1}{\tau s + 1} u$$



Assume: $u(t)=0, y(0)=y_0$

Question: $y(t) ?$

Stability in the time domain

Laplace domain:

$$\frac{y}{u} = \frac{1}{\tau s + 1}$$

$$(\tau s + 1)y = u$$

Time domain:

$$\tau \dot{y} + y = u$$

Solution:

$$\begin{aligned} y(t) &= k e^{\lambda t} \\ \dot{y}(t) &= \lambda k e^{\lambda t} \end{aligned}$$

Initial condition:

$$u=0 \quad y(0)=y_0$$

Substitute in differential equation:

$$\tau \cdot \lambda k e^{\lambda t} + k e^{\lambda t} = 0$$

$$k \neq 0 \quad e^{\lambda t} \neq 0$$

$$(\tau \lambda + 1)k e^{\lambda t} = 0$$

$$\lambda = -\frac{1}{\tau}$$

Initial condition: $y_0 = k \cdot e^{-\frac{1}{\tau} \cdot 0}$

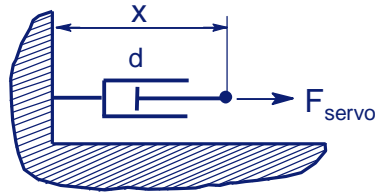
$$y_0 = k$$

$$y(t) = y_0 \cdot e^{-\frac{t}{\tau}}$$

Stability in the time domain

First order system
(damper with P controller):

$$y = \frac{1}{\tau s + 1} u$$



Assume: $u(t)=0, y(0)=y_0$

Question: $y(t) ?$

Solution: $y(t)=y_0 e^{-t/\tau}$

stable if: $\tau > 0!!!$

Intermezzo: poles and zeros

Transfer function examples:

First order system: $H(s) = \frac{1}{\tau s + 1}$

Second order system: $H(s) = \frac{1}{ms^2 + ds + c}$

PD controller: $C(s) = (k_p + k_v s)$

Fourth order system w. zeros: $H(s) = \frac{\omega_o^2 / \omega_n^2}{Ms^2} \frac{s^2 + 2\beta\omega_n s + \omega_n^2}{s^2 + 2\beta\omega_o s + \omega_o^2}$

Standard form:

$$H(s) = K \frac{(s - z_1)(s - z_2) \dots (s - z_m)}{(s - p_1)(s - p_2) \dots (s - p_n)}$$

Intermezzo: poles and zeros

$$H(s) = K \frac{(s - z_1) (s - z_2) \dots (s - z_m)}{(s - p_1) (s - p_2) \dots (s - p_n)}$$

\leftarrow zeros
 \leftarrow poles

Zeros are roots of the numerator polynomial

(values of s for which numerator becomes zero)

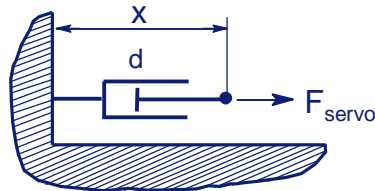
Poles are roots of the denominator polynomial

(values of s for which denominator becomes zero)

n: number of poles = order of the system

Stability in the frequency domain

First order system
(damper with P controller)



Transfer function in standard form:

$$H(s) = \frac{1}{\tau s + 1} = K \frac{1}{(s - p_1)}$$

\leftarrow zeros
 \leftarrow poles

Zero: -

Pole: $\tau s + 1 = 0 \Rightarrow s = -1/\tau$

$p_1 = -1/\tau$ stable if $p_1 < 0$

Poles determine stability!!!

Stability in the frequency domain

Second order system
(mass-spring-damper):

$$H(s) = \frac{1}{ms^2 + ds + c}$$

Transfer function in
standard form:

$$H(s) = \frac{K}{(s - p_1)(s - p_2)}$$

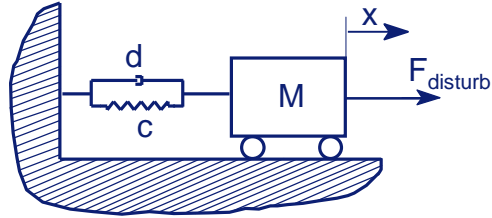
← zeros
← poles

Zero: -

Poles:
$$p_{1,2} = -\frac{1}{2} \frac{d}{m} \pm \frac{1}{2} \sqrt{\frac{d^2}{m^2} - 4 \frac{c}{m}}$$

Stable if $d > 0$, or: $\text{Re}(p) < 0$

Poles determine stability!!!



Stability in the frequency domain

PD controller

$$C(s) = (k_p + k_v s)$$

Transfer function in
standard form:

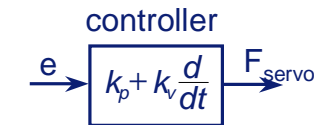
$$C(s) = \frac{K(s - z_1)}{1}$$

← zeros
← poles

Zero: $z_1 = -k_p/k_v$

Pole: -

Always stable



Poles determine stability!!!

Stability in the frequency domain

PD controller in series with mass-spring-damper:

$$C(s)H(s) = \frac{(k_p + k_v s)}{ms^2 + ds + c}$$

Transfer function in standard form:

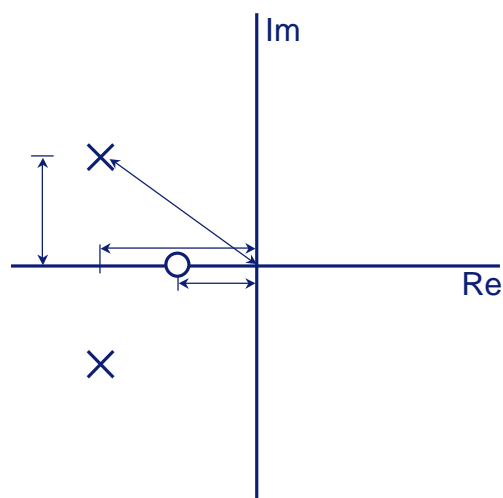
$$C(s)H(s) = \frac{K(s - z_1)}{(s - p_1)(s - p_2)}$$

\leftarrow zeros
 \leftarrow poles

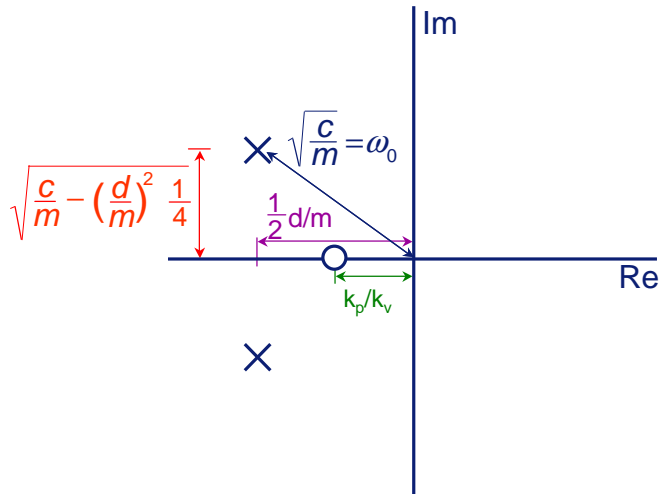
Zero: $z_1 = -k_p/k_v$

Pole: $p_{1,2} = -\frac{1}{2} \frac{d}{m} \pm \frac{1}{2} \sqrt{\frac{d^2}{m^2} - 4 \frac{c}{m}}$

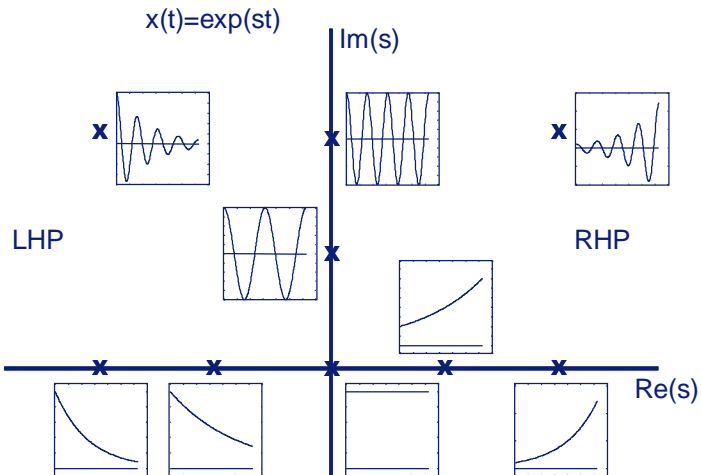
Pole-zero map in s-plane



Pole-zero map in s-plane

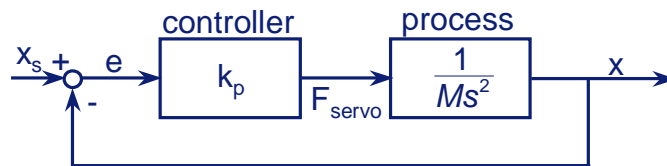


Stability of poles in s-plane

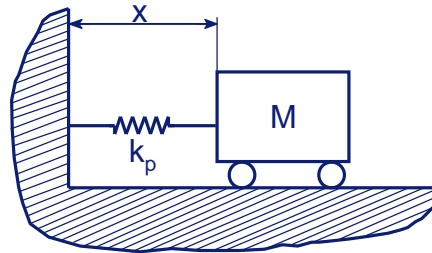


Stability of closed loop systems

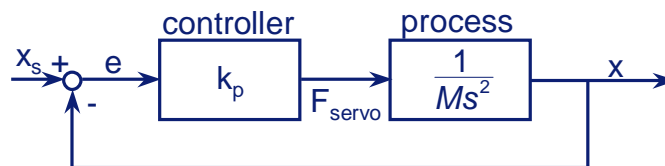
Closed loop system
(simple mass with P controller):



Mechanical equivalent:



Stability of closed loop systems



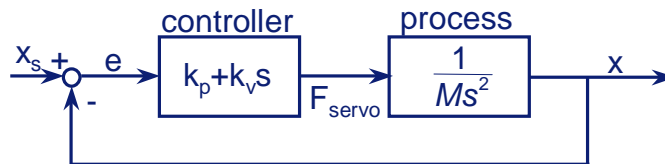
Transfer function:
$$\frac{x}{x_s} = \frac{k_p}{Ms^2 + k_p}$$

Poles: $Ms^2 + k_p = 0$, or

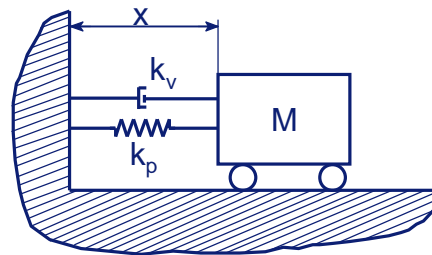
$$s^2 = -\frac{k_p}{M} \Rightarrow s = \pm j\sqrt{\frac{k_p}{M}} \quad \text{Marginally stable!!!}$$

Stability of closed loop systems

Closed loop system
(simple mass with PD controller):



Mechanical equivalent:



Exercise Poles

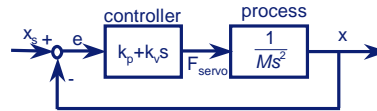
For the controlled mechanical system of the previous slide, take $M=1$ Kg, $k_p=2$ N/m and $k_v=2$ Ns/m.

1. Calculate the poles of the open-loop system.
2. Calculate the poles of the closed-loop system.
3. Is the system stable?

Stability of closed loop systems

Open-loop: $\frac{x}{e} = \frac{k_v s + k_p}{Ms^2} = H(s)$

Closed-loop: $\frac{x}{x_s} = \frac{H(s)}{1 + H(s)}$



$$\frac{x}{x_s} = \frac{H}{1+H} = \frac{\frac{k_v s + k_p}{Ms^2}}{1 + \frac{k_v s + k_p}{Ms^2}} = \frac{k_v s + k_p}{Ms^2 + k_v s + k_p}$$

Closed-loop poles: $1+H(s)=0$, or;

$$Ms^2 + k_v s + k_p = 0 \quad \text{Stable if } k_v > 0$$

Intermezzo: Nyquist plot

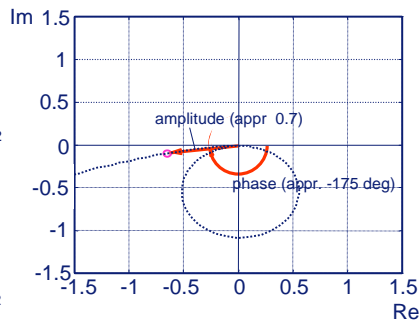
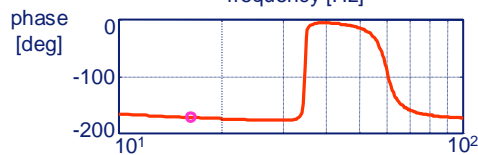
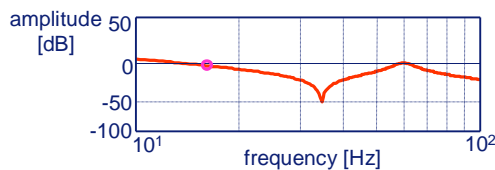
H(s)

Bode plot:

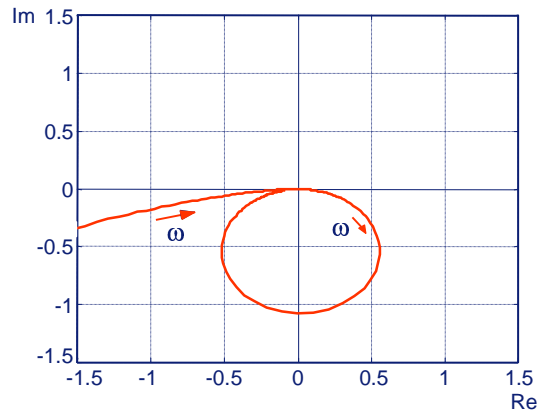
- $\log(|H|)$ vs. $\log(f)$
- $\angle H$ vs. $\log(f)$

Nyquist plot:

- $\text{Re}(H)$ vs. $\text{Im}(H)$
- in complex plane



Intermezzo: Nyquist plot



Exercise Nyquist plots

Make Bode and Nyquist diagrams for the following systems:

1. A mass (double integrator)
2. A double integrator in series with K_p/K_v controller
3. A first order system

Towards the Nyquist stability criterion

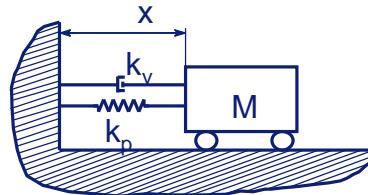
Stability:

- Poles of closed loop system in LHP
- Poles of closed loop are solutions of $1 + H(s) = 0$
- Nyquist plot of open loop $H(s)$ can be used to evaluate stability...

Yet another exercise...

Exercise $s \rightarrow H(s)$ map

For the controlled mechanical system of earlier pages, take $M=1$ Kg, $k_p=2$ N/m and $k_v=2$ Ns/m.

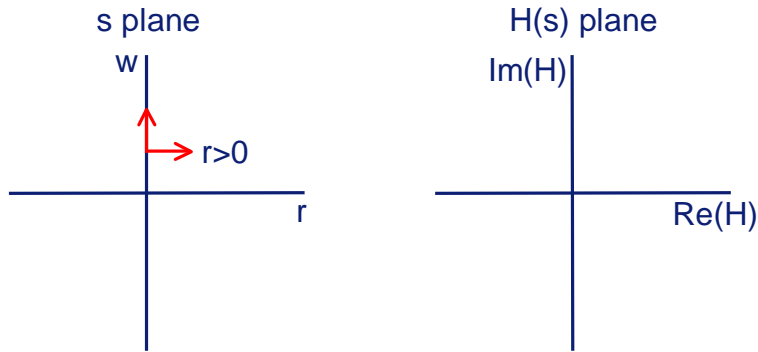


Open-loop:
$$\frac{x}{e} = \frac{k_v s + k_p}{M s^2} = H(s)$$

Closed loop:
$$\frac{x}{x_s} = \frac{H}{1+H} = \frac{k_v s + k_p}{M s^2 + k_v s + k_p}$$

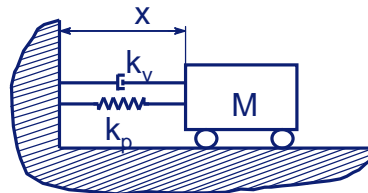
Check if $s=2$ is a solution to $1+H(s)=0$. Same for $s=-2+3j$, $s=-1+j$, $s=-1-j$. Plot these s values in the complex plane (s -plane). Plot the corresponding value of $H(s)$ in another complex plane plot ($H(s)$ plane).

Exercise s→H(s) map



Exercise s→H(s) map

For the controlled mechanical system of earlier pages, take $M=1$ Kg, $k_p=2$ N/m and $k_v=2$ Ns/m.

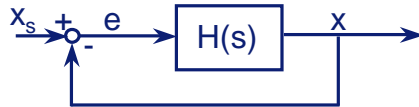


Open-loop: $\frac{x}{e} = \frac{k_v s + k_p}{M s^2} = H(s)$

Closed loop: $\frac{x}{x_s} = \frac{H}{1+H} = \frac{k_v s + k_p}{M s^2 + k_v s + k_p}$

1. Assume that we consider sinus-types of signals, i.e. $s=j\omega$.
Make the $H(s)$ plot for $\omega=0 \dots \infty$.
2. Is the system stable?

Nyquist stability criterion



$$H_c(s) = \frac{H(s)}{1 + H(s)}$$

Stability: check RHP poles of $H_c(s)$

$$1 + H(s) = 0 \quad \text{for } \text{Re}(s) > 0$$

Question:

Given a frequency response $H(j\omega)$, how to check stability?

Answer:

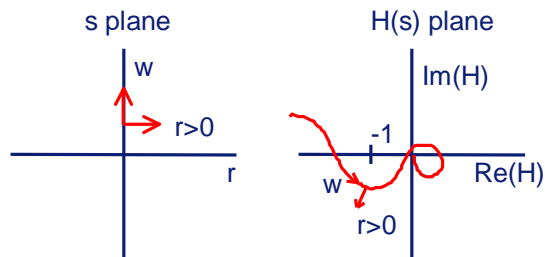
Use Nyquist plot of $H(j\omega)$ in the complex plane, and evaluate with respect to the $(-1, 0)$

Nyquist stability criterion

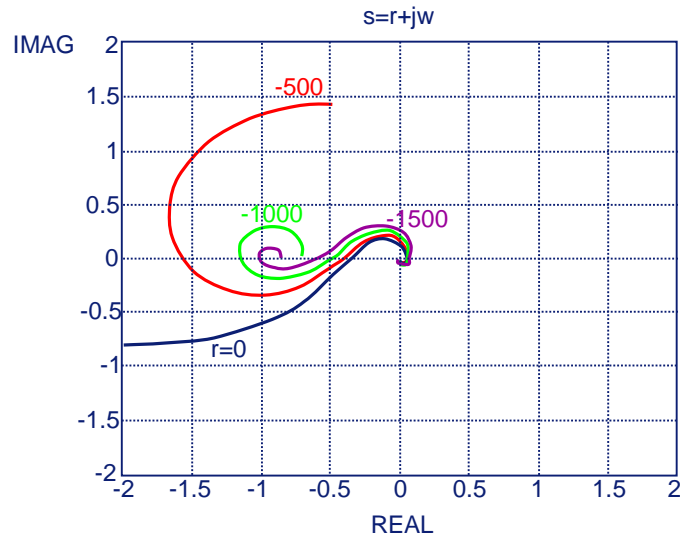
Graphical evaluation of stability

For increasing frequency along the curve of $H(j\omega)$ in the complex plane, the point $(-1, 0)$ should stay at the left hand side of the curve

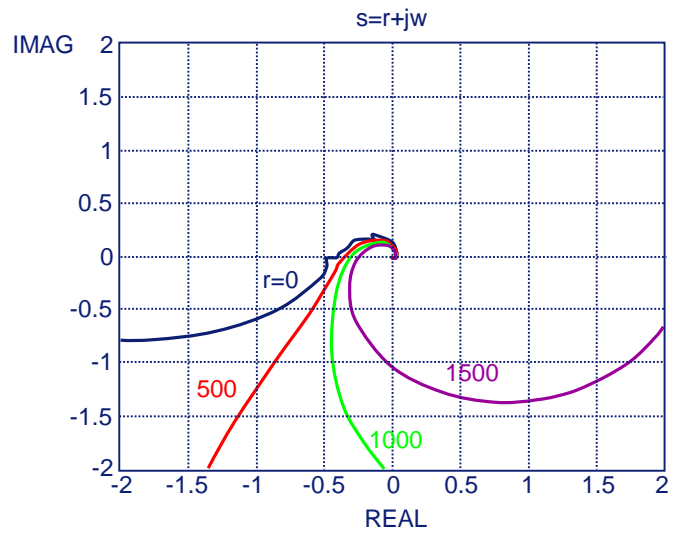
$H(s)$ with $s = r + j\omega$



Nyquist stability criterion

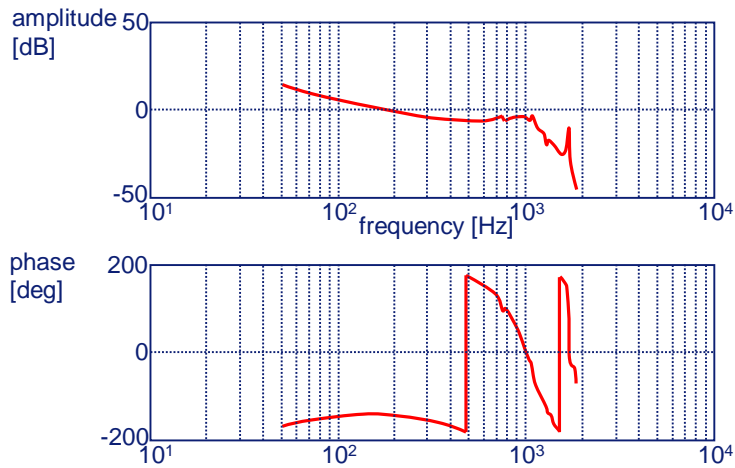


Nyquist stability criterion



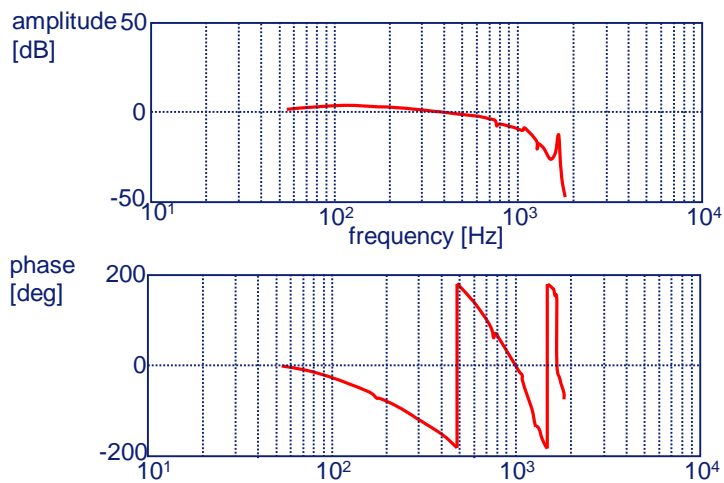
Example of experimental system

Measurement of open loop reticle stage



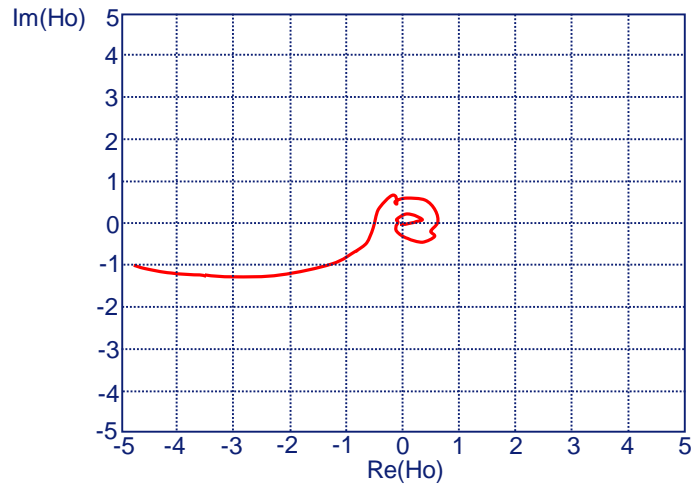
Example of experimental system

Measurement of closed loop reticle stage



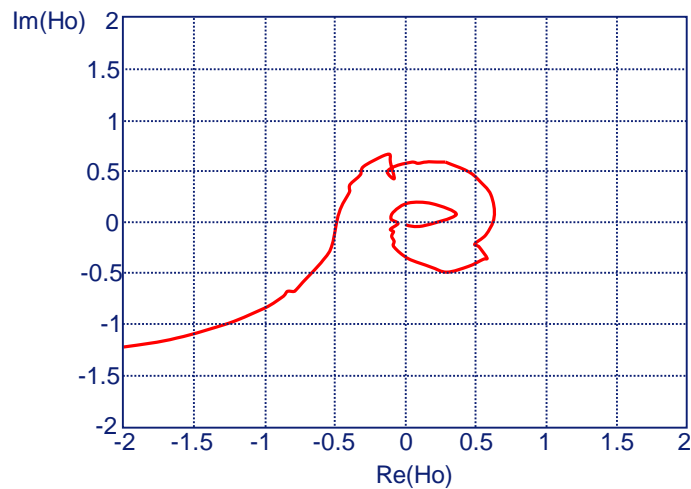
Example of experimental system

Nyquist plot of open loop reticle stage



Example of experimental system

Nyquist plot of open loop reticle stage (zoomed)



Stability margins

Margin = Distance of $H(j\omega)$ to the critical point

Phase Margin (PM) = allowable phase shift up to instability (rotation of $H(j\omega)$ diagram)

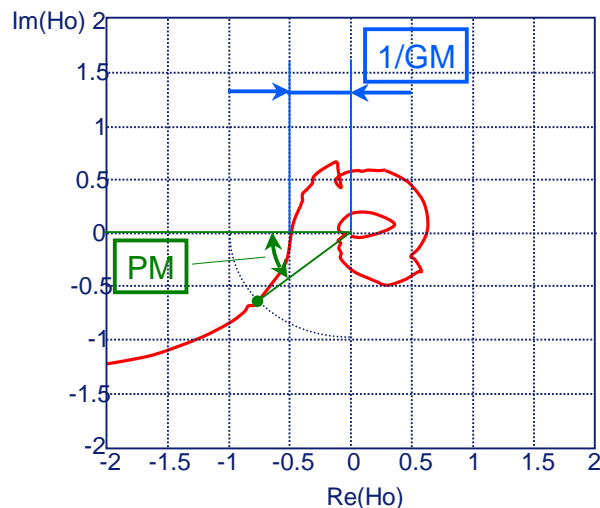
Or: check phase of $H(j\omega)$ where $|H(j\omega)|=1$

Gain Margin (GM) = allowable gain increase up to instability (enlargement of $H(j\omega)$ diagram)

Or: check gain of $H(j\omega)$ where $\angle H(j\omega) = -180^\circ$

Stability margins

Nyquist plot of open loop reticle stage



Summary

- Stability in time domain
- Poles / Zeros
- Stability in frequency domain
 - Poles of closed loop should be in RHP
- The Nyquist plot
- The Nyquist stability criterion
 - Leave $(-1,0)$ at left hand of open loop $H(s)$
 - Leave sufficient stability margins (gain/phase)

